

In this paper we show that problems concerning the development of a boundary layer on a semi-infinite plate when the outer flow speed is of the form $U = (1 + ct)^b a$, and on a cylinder when the outer flow speed has the forms $U = ct^\alpha x^m$ and $U = (1 + ct)^b a x^m$, are self-similar. We present the results of numerical calculations for various values of α , b , and m . We consider the problem of a stepwise nonstationary heating of a plate, impulsively set into motion in an incompressible fluid; we show that this problem is self-similar and obtain its solution numerically.

Problem Concerning the Motion of a Semi-Infinite Plate with Speed $U = (1 + ct)^b a$

In this case the system of differential equations for the nonstationary laminar boundary layer and the associated boundary conditions have the form

$$\begin{aligned} \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} &= 0; \\ \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= acb(1 + ct)^{b-1} + v \frac{\partial^2 u}{\partial y^2}; \\ u=U, v=0 \text{ for } y=0, t=0; \\ u=0, v=0, y=0, t > 0, x > 0; \\ u=U, y=\infty, t > 0, x > 0. \end{aligned} \tag{1}$$

As new independent variables and functions we take the following:

$$\xi = \frac{x}{(1 + ct)^{1+b}}; \quad \eta = \frac{y}{(1 + ct)^{1/2}}; \quad u = \Phi(1 + ct)^b; \quad v = \frac{V}{(1 + ct)^{1/2}}.$$

With these substitutions the problem may be written in the form

$$\begin{aligned} \frac{\partial \Phi}{\partial \xi} + \frac{\partial V}{\partial \eta} &= 0; \\ bc\Phi - \frac{1}{2} c\eta \frac{\partial \Phi}{\partial \eta} - c(1 + b)\xi \frac{\partial \Phi}{\partial \xi} + \Phi \frac{\partial \Phi}{\partial \xi} + V \frac{\partial \Phi}{\partial \eta} &= acb + v \frac{\partial^2 \Phi}{\partial \eta^2}; \\ \Phi(\eta, \xi) &= 0, V=0 \text{ for } \eta=0; \\ \Phi(\eta, \xi) &= 1 \text{ for } \eta=\infty. \end{aligned}$$

Problem Concerning Acceleration of a Cylinder ($U = ct^\alpha x^m$)

The system of boundary-layer equations (see [1]) has the form

$$\begin{aligned} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= \alpha c x^m t^{\alpha-1} + c^2 t^{2\alpha} m x^{2m-1} + v \frac{\partial^2 u}{\partial y^2}; \\ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} &= 0. \end{aligned} \tag{2}$$

Leningrad. Translated from Zhurnal Prikladnoi Mekhaniki i Tekhnicheskoi Fiziki, No. 4, pp. 122-125, July-August, 1975. Original article submitted October 31, 1974.

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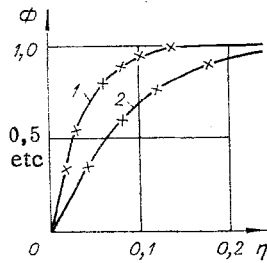


Fig. 1

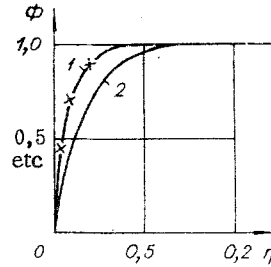


Fig. 2

The boundary conditions here are analogous to the conditions in problem (1). We introduce the new variables

$$\xi = x \left(\frac{\alpha+1}{t^{1-m}} \right)^{-1}, \quad \eta = \frac{y}{t^{1/2}};$$

$$\Phi = u/cx^m t^{-\alpha}, \quad V = v/cx^{m-1} t^{-(\alpha+1/2)}.$$

In terms of these new variables Eqs. (2) become

$$\alpha\Phi + \frac{(\alpha+1)}{m-1} \xi \frac{\partial\Phi}{\partial\xi} - \frac{1}{2} \eta \frac{\partial\Phi}{\partial\eta} + \Phi \left[cm\xi^{m-1} \Phi + c\xi^m \frac{\partial\Phi}{\partial\xi} \right] + c\xi^{m-1} V \frac{\partial\Phi}{\partial\eta} = \alpha + cm\xi^{m-1} + v \frac{\partial^2\Phi}{\partial\eta^2};$$

$$m\Phi + \xi \frac{\partial\Phi}{\partial\xi} + \frac{\partial V}{\partial\eta} = 0,$$

while the boundary conditions have the same form as in problem (1).

To solve this problem numerically we use the implicit numerical scheme (see [2]).

$$\frac{\Phi_i^{j+1} - \Phi_i^j}{\Delta\xi} = \frac{1}{\left(\Phi_i^{j+1} c\xi_i^m + \frac{\alpha+1}{m-1} \xi_i \right)} \left[\frac{\Phi_{i+1}^{j+1} - 2\Phi_i^{j+1} + \Phi_{i-1}^{j+1}}{\Delta\eta^2} - \left(c\xi_i^{m-1} V_i^{j+1} - \frac{1}{2} \eta_i \right) \frac{\Phi_{i+1}^{j+1} - \Phi_i^{j+1}}{\Delta\eta} + cm\xi_i^{m-1} (1 - \Phi_i^{j+1})^2 + \alpha (1 - \Phi_i^{j+1}) \right].$$

In calculating the flow field in the direction of the longitudinal coordinate η we use the driver method at each i -th point ξ_i . Figures 1 and 2 show the tangential velocity component for the ξ, η coordinate values used in the computations with the c value taken equal to 500 (in these figures curves 1 and 2 correspond to ξ values of 0.5 and 11, respectively). Figure 1 is for the case $\alpha = 0.5$ and $m = 0.5$; Fig. 2 is for $\alpha = 0.5$ and $m = 1.5$. The starred points are for $\alpha = 1.5$ and $m = 0.5$ in Fig. 1; in Fig. 2 they are for $\alpha = 1.5$ and $m = 1.5$. From the difference scheme used and from the graphs it is evident that the exponent α depends weakly on the dimensionless velocity profile, while m changes its form completely depending on the coordinates.

Problem Concerning the Motion of a Cylinder with the Speed $U = (1 + ct)^b \alpha x^m$

With the introduction of the variables

$$\xi = \frac{x}{(1+ct)^{\frac{1+b}{1-m}}}; \quad \eta = \frac{y}{(1+ct)^{1/2}}; \quad \Phi = \frac{u}{\alpha x^m} (1+ct)^{-b};$$

$$V = \frac{v}{cx^{m-1}} (1+ct)^{-\left(\frac{1}{2}+b\right)}$$

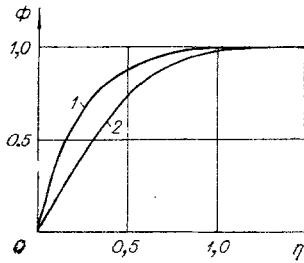


Fig. 3

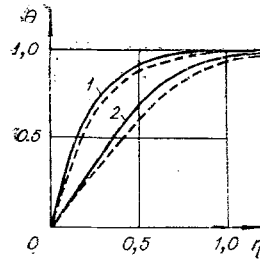


Fig. 4

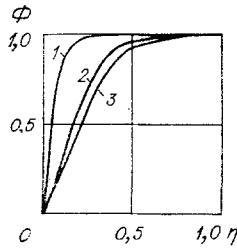


Fig. 5

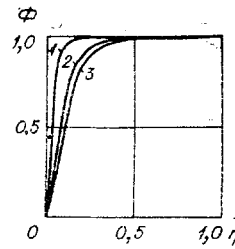


Fig. 6

this problem may be written in the form

$$bc\Phi - \frac{1}{2}c\eta \frac{\partial\Phi}{\partial\eta} - \frac{1+b}{1-m}c\xi \frac{\partial\Phi}{\partial\xi} + \Phi \left[a\xi^m \frac{\partial\Phi}{\partial\xi} + ma\xi^{m-1}\Phi \right] + \\ + a\xi^{m-1}V \frac{\partial\Phi}{\partial\eta} = bc + am\xi^{m-1} + v \frac{\partial^2\Phi}{\partial\eta^2}; \quad m\Phi + \xi \frac{\partial\Phi}{\partial\xi} + \frac{\partial V}{\partial\eta} = 0; \\ \Phi(\eta, \xi) = 0, \quad V = 0 \quad \text{for } \eta = 0; \\ \Phi(\eta, \xi) = 1 \quad \text{for } \eta = \infty.$$

Since in the initial equations only the derivative with respect to t appears, we can state that if there is self-similarity for the functions $U = f(t)\varphi(x)$, there will also be self-similarity for the function $U = f(1 + ct)\varphi(x)$.

The numerical scheme used to obtain a solution is similar to that of the previous problem. An analysis of the results confirms the weak influence of the acceleration law which applies here; it also confirms the strong dependence of the dimensionless velocity profile on the form of the body (m).

The equations describing the problem concerning stepwise nonstationary heating of a flat plate, set impulsively into motion, are (see [1])

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0; \\ \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = v \frac{\partial^2 u}{\partial y^2}; \\ \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{v}{\sigma} \frac{\partial^2 T}{\partial y^2}, \quad (3)$$

where σ is the Prandtl number, and

$$u = v = 0, \quad T = T_e \quad \text{for } t = 0;$$

$$\begin{array}{ll}
u=v=0 & \text{for } t > 0, y=0; \\
u=U_\infty & \text{for } t > 0, x > 0, y=\infty; \\
T=T_w & \text{for } t > 0, y=0, x > 0; \\
T=T_e & \text{for } t > 0, y=\infty.
\end{array}$$

After substituting the variables

$$u = \Phi(\xi, \eta); \quad v = \frac{\Gamma}{t^{1/2}}; \quad \xi = \frac{x}{t}; \quad \eta = \frac{y}{t^{1/2}}; \quad \theta = \frac{T - T_w}{T_e - T_w}$$

we can rewrite problem (3) in the form

$$\begin{aligned}
& \frac{\partial \Phi}{\partial \xi} + \frac{\partial V}{\partial \eta} = 0; \\
& -\xi \frac{\partial \Phi}{\partial \xi} - \frac{1}{2} \eta \frac{\partial \Phi}{\partial \eta} + \Phi \frac{\partial \Phi}{\partial \xi} + V \frac{\partial \Phi}{\partial \eta} = \nu \frac{\partial^2 \Phi}{\partial \eta^2}; \\
& -\xi \frac{\partial \theta}{\partial \xi} - \frac{1}{2} \eta \frac{\partial \theta}{\partial \eta} + \Phi \frac{\partial \theta}{\partial \xi} + V \frac{\partial \theta}{\partial \eta} = \frac{\nu}{\sigma} \frac{\partial^2 \theta}{\partial \eta^2}; \\
& \Phi = V = 0, \quad \theta = 0, \quad \eta = 0; \\
& \Phi = U, \quad \theta = 1, \quad \eta = \infty.
\end{aligned}$$

The kinematic and temperature profiles for $U_\infty = 500$ cm/sec are shown in Figs. 3 and 4 for $\sigma = 0.7$ (solid curve) and $\sigma = 0.4$ (dashed curve), respectively. Curves 1 and 2 correspond to ξ values of 0.25 and 17.75, respectively.

We employed the same methods to analyze the thermal boundary layer in the presence of a longitudinal pressure drop (impulsive Falkner-Skan motion) for small Mach numbers. The calculated results are shown in Figs. 5 and 6 for $m = 0.5$ and $\sigma = 0.7$, where the curves 1, 2, and 3 correspond to ξ values of 0.25, 17.75, and 37, respectively.

For the Falkner-Skan problem the thermal and kinematic profiles differ considerably from one another.

By using the self-similar variables we can carry out the calculations on a machine like the BESM-3M, a stationary solution being obtained after a computer time of some 20 to 30 min. One can also show, within the scope of the boundary-layer theory, that the problem concerning the impulsive motion of a plate in a compressible gas, as well as the problem concerning the formation of a boundary layer behind a transient shock wave on a thin semi-infinite plate, is self-similar.

LITERATURE CITED

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